Introduction

High resolution imaging is important for accurate characterization of pathological abnormalities of biomedical specimens. Given the excellent axial resolution in three-dimensional (3D) imaging (1-4), optical coherence tomography (OCT) has been extensively used in ophthalmic imaging, vascular medicine, dermatological study, etc. Lateral resolution of the OCT is light diffraction limited, which precludes the feasibility of quantitative assessment of individual cells. In this paper, we demonstrated the feasibility of breaking diffraction-limit in OCT imaging through virtually structured detection (VSD). OCT examination of optical resolution target verified resolution doubling in the VSD based OCT imaging. Super-resolution OCT identification of individual frog photoreceptors was demonstrated to verify the potential of resolution enhancement in retinal imaging. We anticipate that further development of the VSD based OCT promises an easy, low cost strategy to achieve sub-cellular resolution tomography of the retina and other biological systems.

Keywords: Optical coherence tomography (OCT); retina; three-dimensional imaging

Abstract: Quantitative imaging of biomedical specimens is essential in biomedical study and diagnosis. Given excellent capability in three-dimensional (3D) imaging, optical coherence tomography (OCT) has been extensively used in ophthalmic imaging, vascular medicine, dermatological study, etc. Lateral resolution of the OCT is light diffraction limited, which precludes the feasibility of quantitative assessment of individual cells. In this paper, we demonstrated the feasibility of breaking diffraction-limit in OCT imaging through virtually structured detection (VSD). OCT examination of optical resolution target verified resolution doubling in the VSD based OCT imaging. Super-resolution OCT identification of individual frog photoreceptors was demonstrated to verify the potential of resolution enhancement in retinal imaging. We anticipate that further development of the VSD based OCT promises an easy, low cost strategy to achieve sub-cellular resolution tomography of the retina and other biological systems.

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Field illumination is not suitable for scanning laser imaging modalities, such as OCT. In theory, an alternative strategy to the SIM is to combine spatial and temporal modulations, either by spatiotemporal modulation of the scanning laser profile (in the illumination path) or the recording light profile (in the detection path) (19). However, physical implementation of the illumination/detection modulation is difficult. So far, experimental validation of the proposed spatiotemporal modulation is not yet demonstrated. We recently demonstrated a virtually structured detection (VSD) based super-resolution scanning laser microscopy (SLM) to achieve resolution doubling (20). Without the complexity of structured illumination, VSD provides an easy, low-cost and phase-artifact free strategy to achieve super-resolution imaging. The purpose of this study is to demonstrate the feasibility of breaking diffraction-limited resolution in OCT imaging through VSD. OCT examination of optical resolution target verified resolution enhancement in the VSD based imaging. Super-resolution OCT identification of individual frog photoreceptors was validated to demonstrate the potential of resolution enhancement in retinal imaging. We anticipate that further development of the VSD based OCT can provide an easy, low cost strategy to achieve sub-cellular resolution tomography of the retina and other biological systems.

**Materials and methods**

**Experimental setup**

*Figure 1* shows the diagram of the VSD based super-resolution OCT. A near infrared superluminescent diode (SLD-351, Superlum) with a center wavelength λ =830 nm and band width Δλ =60 nm was used to illuminate the sample. A dual-axis galvo (GVS002, Thorlabs) was used to scan the focused illuminating light across the sample in a raster pattern and descan light reflected from sample to the light detector. We used a two-dimensional (2D) digital camera (Pike F-032B, Allied Vision Technologies) to replace the single element sensor in conventional time-domain OCT. In the reference arm, neutral density filters were applied to adjust light intensity. A glass block was inserted into the reference arm to compensate for optical dispersion (21) of the electro-optic phase modulator (EOM, Model 350-50, Conoptics), which was employed to introduce rapid vibration free phase modulation for OCT reconstruction (22). Briefly, EOM shifted reference beam light phase by 0, π/2, π and 3π/2 at each scanning position. Four corresponding interference patterns were recorded at each scanning position for OCT reconstruction. The axial resolution of the system was ~4 μm (0.44 \( \lambda^2 / n \Delta \lambda \), where \( n \) was the refractive index of the sample, ~1.4). With a 0.1 NA 5× objective, lateral resolution of conventional OCT was theoretically estimated at ~5 μm (0.61 \( \lambda / \text{NA} \)). In theory, the VSD can improve the resolution by a factor of 2 (19,20,23). A virtual pinhole (two times of the Airy disc diameter) was applied during reconstruction.

**Principle of the VSD based OCT**

For simplicity, formulas will be written in one-dimension. During the OCT recording, the reference mirror was adjusted to a position where the zero delay plane is superimposed with the focal plane. First, the standard four-frame phase-shifting algorithm is applied to retrieve OCT images (24). By ignoring optical magnification, the interference pattern (in X direction) recorded by the camera at a given scanning position \( x_0 \) is

\[
I(x,x_0) = I_a(x,x_0) + I_b(x) + 2\sqrt{I_a(x,x_0)I_b(x)} \cos[\theta(x,x_0) + \delta_b] \tag{1}
\]
where $I_s$ is the intensity distribution of light reflected from sample, $I_R$ is the intensity distribution of light reflected from mirror in the reference arm, $\theta$ is the time-invariant phase difference distribution between the sampling arm and the reference arm, $i = 1, 2, 3, 4$ and $\delta_i$ is the phase modulation item:

$$\delta_i = (i - 1)\pi / 2$$

According to the standard four-frame phase-shifting algorithm (24), we will have

$$I_s(x, y) = \frac{[I_s(x, y) - I_s(x, y)]^2 + [I_s(x, y) - I_s(x, y)]^2}{I_s(x)} [3]$$

If we assume the reference intensity profile is spatially invariant within the virtual pinhole:

$$I_R(x) = c$$

and constant coefficients are ignored, the Eq. [3] can be simplified as:

$$I_s(x, y) = [I_s(x, y) - I_s(x, y)]^2 + [I_s(x, y) - I_s(x, y)]^2$$

The second step is to apply VSD to break through diffraction limit of lateral resolution. Details of VSD have been reported in our recent publication (20). Briefly, a digital sinusoidal mask $m(x)$ is applied to multiply with the OCT profile map:

$$I_{mul}(x, y) = I_s(x, y) \cdot m(x)$$

The spatial integral of Eq. [6] yields:

$$p(x_0) = \int I_{mul}(x, y) \, dx$$

$$= h_{il}(x_0) \otimes s(x_0) [h_{de}(x_0) \otimes m(x_0)]$$

where $h_{il}$ and $h_{de}$ are PSFs of the illumination beam and detection beam, respectively, and $s$ is the reflectance ratio of the sample. Fourier transforming Eq. [7] yields:

$$\tilde{p}(f_x) = \tilde{h}_{il}(f_x) \tilde{s}(f_x) \otimes \tilde{h}_{de}(f_x) \otimes \tilde{m}(f_x)$$

We can see that if the carrier frequency of $\tilde{m}$ is smaller than the cutoff frequency of $\tilde{h}_{de}$, the convolution in Eq. [8] can shift the high frequency of the sample toward the lower frequency to pass through $\tilde{h}_{il}$, thus to break through diffraction limited resolution.

**Sample preparation**

We used a standard optical resolution target (USAF 1951 1X, Edmond) and freshly isolated frog (Rana Pipiens) for experimental validation of the proposed VSD based OCT system. The optical resolution target provided a simple sample for technical validation of the OCT resolution. In contrast to simple optical target, frog retina had relatively complex 3D structures. The diameter of frog photoreceptor rod was 5-8 μm and that of cone was about 1-3 μm (25,26), which provided an excellent model to test OCT resolution before (5 μm) and after (2.5 μm) VSD data processing. All animal handling procedure was approved by the Institutional Animal Care and Use Committee of the University of Alabama at Birmingham. Frog used for preparing freshly isolated retina was firstly euthanized by rapid decapitation and double pithing. Then eyeball was detached and moved to Ringer’s solution [containing (27) in mmol/L: 110 NaCl, 2.5 KCl, 1.6 MgCl$_2$, 1.0 CaCl$_2$, 22 NaHCO$_3$, and 10 D-glucose]. After hemisecting the eyeball with fine scissors, lens was removed and the retina was separated from the eyecup. Dissected retina was then moved to a chamber filled with Ringer’s solution for image recording. All procedure was conducted in a dark room illuminated with dim red light.

**Results**

**Super-resolution OCT imaging of optical resolution target**

Figure 2 compares conventional OCT image and the VSD based OCT image of the optical resolution target. The smallest grating of the optical resolution target had a period of 4.4 μm. Since the lateral resolution of the conventional OCT system was 5 μm, the smallest grating could not be resolved by conventional OCT as indicated by the white arrow in Figure 2A. Moreover, it was difficult for conventional OCT to differentiate the second smallest grating which has a period of 4.9 μm (blue arrow in Figure 2A). In contrast, the VSD based OCT was capable of resolving both the smallest grating (white arrow in Figure 2B) and the second smallest grating (blue arrow in Figure 2B). The normalized intensity profile in Figure 2C confirmed the resolution enhancement of the VSD based OCT. Three clear bumps corresponding to the second smallest grating (blue dashed rectangle in Figure 2C) and three bumps corresponding to the smallest grating (white dashed rectangle in Figure 2C) manifested themselves more clearly after VSD reconstruction.

**Super-resolution OCT imaging of freshly isolated retina**

After we tested super-resolution OCT using the optical
resolution target, we implemented super-resolution OCT imaging of freshly isolated frog retina. Figure 3A shows a cross-section image of freshly isolated frog retina acquired by conventional OCT. With ~4 μm axial resolution, we could clearly see retinal layer structure which consisted of inner plexiform layer (IPL), inner nuclear layer (INL), outer plexiform layer (OPL), outer nuclear layer (ONL) and photoreceptor layer (PRL). Enface images were acquired at the inner segment of PRL (yellow dashed line in Figure 3A) which rendered strong OCT signal and rich structure details. Comparing Figure 3B to Figure 3C, we can see that in Figure 3C more cellular structures could be observed. For example, three individual photoreceptors could be identified (three white arrows in Figure 3C), while only a single blur structure could be visualized at the same area in Figure 3B. Resolution enhancement was also confirmed by comparing light intensity profiles. The green and red curves in Figure 3D corresponded to normalized intensity profiles along the green line in Figure 3B and the red line in Figure 3C, respectively. Two individual cells were separated on the red curve (white arrows in Figure 3D), while they merged together on the green curve.

**Discussion**

In summary, we demonstrated that VSD can be implanted...
in OCT imaging to break through the diffraction limit. OCT imaging of optical resolution target (Figure 2) and frog retinal photoreceptors (Figure 3) showed noticeable resolution improvement. Detailed structures that were not identified in conventional OCT images could be readily resolved in super-resolution OCT images through the VSD. Although the VSD based method can be implemented in an imaging system with a high magnification objective, we selected a relatively low magnification objective (5×) in this study for technical validation of super-resolution imaging of frog photoreceptors. Since frog retina consists of photoreceptors with variable diameters (rods: ~5-8 μm; cones: ~1-3 μm) (26,27), it provided an excellent preparation to evaluate the OCT resolution before (5 μm) and after (2.5 μm) VSD data processing.

During VSD reconstruction, the virtual pinhole size was set to two times of the Airy disc diameter. Within the virtual pinhole, we assumed the intensity profile of the light from the reference arm was uniform, as shown in Eq. [4]. However, the actual light intensity attenuated away from the center and became weak at the edge of the virtual pinhole. In other words, the virtual pinhole was truncated by the reference light profile. Therefore, the effective pinhole size became smaller. A smaller confocal pinhole (i.e., <1 Airy disc diameter) can in theory improve the lateral resolution in a confocal system (28). However, with a smaller effective pinhole size, some information was lost for VSD reconstruction. One method to readily alleviate the attenuation of the reference light intensity is to insert an aperture at the reference beam. Since the reference light beam size is smaller, the diffraction map, which is the Fourier Transform of the parallel reference light, becomes larger. Therefore, the diffraction profile will become more uniform at the center. An alternative solution is to use a fiber splitter and feed one port to the sampling arm and the other to the reference arm. With this configuration, it is possible to focus the sampling light beam to the camera while maintaining the parallelism of the reference light beam.

The imaging speed of our current super-resolution OCT is relatively slow (40 s per frame). The VSD imposes a spatially resolved detector to record the diffraction profile of each scanning position, which is time-consuming and infeasible for in vivo retinal imaging due to possible eye movements during the recording. Currently, we are integrating a microlens array (MLA) based multifocal scanning system (29) to improve the speed of super-resolution OCT imaging. We anticipate that further development of the VSD based OCT can provide a practical strategy to achieve super-resolution in in vivo OCT imaging of retinal structures.

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**References**


